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## SOLAR PV BASED ZETA CONVERTER WITH FUZZY LOGIC CONTROLLER FED BLDC MOTOR FOR WATER PUMPING APPLICATIONS

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**ABSTRACT:** In this paper Fuzzy controller based for single array fed BLDC motor for water pumping applications is presented. Of the various renewable energy sources, Solar Photovoltaic is one among the cheapest and widely used. Maximum Power Point Techniques are used to extract the maximum power from a PV module and the fuzzy based MPPT technique has been found to provide better results for randomly varying atmospheric conditions as compared to other methods. This paper deals with the utilization of a ZETA converter in solar PV array based water pumping as an intermediate DC-DC converter between a solar PV array and a voltage source inverter (VSI) in order to achieve the maximum efficiency of the solar PV array and the soft starting of the permanent magnet brushless DC (BLDC) motor by proper control. A Zeta converter is a fourth-order DC-DC converter made up of two inductors and two capacitors and capable of operating in either step-up or step-down mode. A BLDC motor is employed to drive a centrifugal type of water pump because its load characteristic is well matched to the maximum power locus of the PV generator. Further to add to its features minimal rule based fuzzy logic speed controller is introduced. The performance characteristics of the proposed drive system are obtained for different operating conditions. The total system performance can be evaluated by using MATLAB/SIMULINK software.

**KEY WORDS:** Brushless dc (BLDC) motor, incremental conductance maximum power point tracking (INC-MPPT), solar photovoltaic (SPV) array, voltage-source inverter (VSI), water pump, zeta converter, Fuzzy logic controller.

### I. INTRODUCTION

The extreme decrease in the cost of power electronic devices and destruction of fossil fuels in not so distant future welcome to utilize the sun based photovoltaic (SPV) created electrical vitality for different applications quite far. The water pumping, an independent use of the SPV cluster produced power is accepting wide

consideration now a days for water system in the fields, family unit applications and mechanical utilize. Albeit a few inquires about have been completed in a territory of SPV cluster sustained water pumping, joining different DC-DC converters and motor drives, the zeta converter in relationship with a

changeless magnet brushless DC (BLDC) motor is not investigated exactly so far to grow such sort of system. Be that as it may, the zeta converter has been utilized as a part of some other SPV based applications[1] besides topology of SPV array encouraged BLDC motor driven water pump with zeta converter has been accounted for and its noteworthiness has been introduced pretty much in [2] in any case, an exploratory approval is missing and the nonattendance of broad writing survey and correlation with the current topologies, have disguised the specialized commitment and inventiveness of the revealed work. The benefits of both BLDC motor and zeta converter can add to build up a SPV array fed water pumping system having a capability of working agreeably under progressively changing environmental conditions. The BLDC motor has high unwavering quality, high proficiency, high torque/inertia ratio, enhanced cooling, low radio recurrence obstruction and clamor and requires for all intents and purposes no [3-4]then again a zeta converter shows taking after preferences over the customary buck, help, buck-support converters and Cuk converter when utilized in SPV based applications. In this paper, fuzzy logic controller (FLC) is used for the control of the speed of the BLDC motor. The speed controllers are the conventional PI controllers and current controllers are the P controllers to achieve high performance drive. Fuzzy logic can be considered as a mathematical theory combining multi-valued logic, probability theory, and artificial intelligence to simulate the human approach in the solution of various problems by using an approximate reasoning to relate different data sets and to make decisions [8].

The Landsman converter is designed to operate always in continuous conduction mode (CCM) irrespective of the variation in irradiance level, resulting in a reduced stress on its power devices and components [9-13]. The speed of BLDC motor is controlled by variation in the DC-link voltage. No additional phase current sensors, additional control or associated circuitry are imposed unlike for the speed control [14-15]. The motor always attains the required speed to pump the water irrespective of the atmospheric variation. By using fuzzy logic controller for BLDC motor the various performances of the proposed water pumping system are analyzed through simulated results in MATLAB/SIMULINK software. The existing literature exploring SPV array-based BLDC motor-driven water pump is based on a configuration shown in Fig.1. A dc-dc converter is used for MPPT of an SPV array as usual. Two phase currents are sensed along with Hall signals feedback for control of BLDC motor, resulting in an increased cost. The additional control scheme causes increased cost and complexity, which is required to control the speed of BLDC motor. Moreover, usually a voltage-source inverter (VSI) is operated with high-frequency PWM pulses, resulting in an increased switching loss and hence the reduced efficiency.

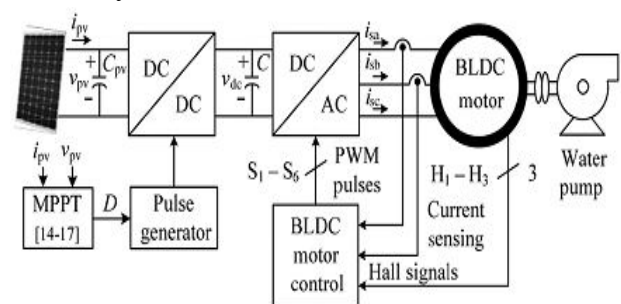


Fig.1. Conventional SPV-fed BLDC motor-driven water pumping system

## II. CONFIGURATION OF PROPOSED SYSTEM

The structure of proposed SPV array-fed BLDC motor driven water pumping system employing a zeta converter is shown in Fig.2. The proposed system consists of (left to right) an SPV array, a zeta converter, a VSI, a BLDC motor, and a water pump. The BLDC motor has an inbuilt encoder. The pulse generator is used to operate the zeta converter. A step-by-step operation of proposed system is elaborated in Section III in detail.

## III. OPERATION OF PROPOSED SYSTEM

The SPV array generates the electrical power demanded by the motor-pump. This electrical power is fed to the motor pump via a zeta converter and a VSI. The SPV array appears as a power source for the zeta converter as shown in Fig.2. Ideally, the same amount of power is transferred at the output of zeta converter which appears as an input source for the VSI. In practice, due to the various losses associated with a dc-dc converter, slightly less amount of power is transferred to feed the VSI. The pulse generator generates, through INCMPPT algorithm, switching pulses for insulated gate bipolar transistor (IGBT) switch of the zeta converter. The INC-MPPT algorithm uses voltage and current as feedback from SPV array and generates an optimum value of duty cycle. Further, it generates actual switching pulse by comparing the duty cycle with a high-frequency carrier wave. In this way, the maximum power extraction and hence the efficiency optimization of the SPV array is accomplished. The VSI, converting dc output from a zeta converter into ac, feeds the BLDC motor to drive a water pump coupled to its shaft. The VSI is operated in fundamental frequency switching through an

electronic commutation of BLDC motor assisted by its built-in encoder. The high frequency switching losses are thereby eliminated, contributing in an increased efficiency of proposed water pumping system.

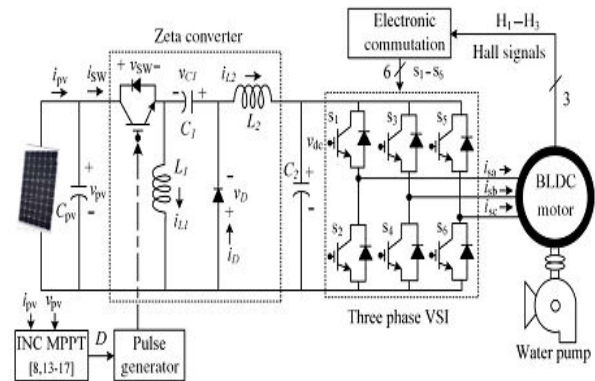


Fig.2. Proposed SPV-zeta converter-fed BLDC motor drive for water pump

## IV. DESIGN OF PROPOSED SYSTEM

Various operating stages shown in Fig.2 are properly designed to develop an effective water pumping system, capable of operating under uncertain conditions. A BLDC motor of 2.89-kW power rating and an SPV array of 3.4-kW peak power capacity under standard test conditions (STC) are selected to design the proposed system. The detailed designs of various stages such as SPV array, zeta converter, and water pump are described as follows.

### A. Design of SPV Array

As per above discussion, the practical converters are associated with various power losses. In addition, the performance of BLDC motor-pump is influenced by associated mechanical and electrical losses. To compensate these losses, the size of SPV array is selected with slightly more peak power capacity to ensure the satisfactory operation regardless of power losses. Therefore, the SPV array of peak power capacity of  $P_{mpp}=3.4$  kW under STC

(STC: 1000 W/m<sup>2</sup>, 25°C, AM 1.5), slightly more than demanded by the motor-pump is selected and its parameters are designed accordingly. Solar World makes Sun module Plus SW 280 mono SPV module is selected to design the SPV array of an appropriate size. Electrical specifications of this module are listed in Table 1 and numbers of modules required to connect in series/parallel are estimated by selecting the voltage of SPV array at MPP under STC as  $V_{mpp} = 187.2V$ .

**TABLE1**  
Specifications of Sun module plus SW 280monoSPV Module

Peak power, $P_m$ (W)	280
Open circuit voltage, $V_o$ (V)	39.5
Voltage at MPP, $V_m$ (V)	31.2
Short circuit current, $I_s$ (A)	9.71
Current at MPP, $I_m$ (A)	9.07
Number of cells connected in series, $N_{sf}$	60

The current of SPV array at MPPI<sub>mpp</sub> is estimated as

$$I_{mpp} = P_{mpp}/V_{mpp} = 3400/187.2 = 18.16 \text{ A} \quad (1)$$

The numbers of modules required to connect in series are as follows:

$$N_s = V_{mpp}/V_m = 187.2/31.2 = 6. \quad (2)$$

The numbers of modules required to connect in parallel are as follows:

$$N_p = I_{mpp}/I_m = 18.16/9.07 = 2. \quad (3)$$

Connecting six modules in series, having two strings in parallel, an SPV array of required size is designed for the proposed system.

## B. Design of Zeta Converter

The zeta converter is the next stage to the SPV array. Its design consists of an estimation of various components such as input inductor  $L_1$ , output inductor  $L_2$ , and intermediate capacitor  $C_1$ . These components are designed such that the zeta converter always operates in CCM resulting in reduced stress on its components and devices. An estimation of the duty cycle  $D$  initiates the design of zeta converter which is estimated as [6]

$$D = \frac{V_{dc}}{V_{dc} + V_{mpp}} = \frac{200}{200 + 187.2} = 0.52 \quad (4)$$

Where  $V_{dc}$  is an average value of output voltage of the zeta converter (dc link voltage of VSI) equal to the dc voltage rating of the BLDC motor.

An average current flowing through the dc link of the VSII<sub>dc</sub> is estimated as

$$I_{dc} = P_{mpp}/V_{dc} = 3400/200 = 17 \text{ A}. \quad (5)$$

Then,  $L_1$ ,  $L_2$ , and  $C_1$  are estimated as

$$L_1 = \frac{DV_{mpp}}{f_{sw}\Delta I_{L1}} = \frac{0.52 \times 187.2}{20000 \times 18.16 \times 0.06} = 4.5 \times 10^{-3} \approx 5 \text{ mH} \quad (6)$$

$$L_2 = \frac{(1-D)V_{dc}}{f_{sw}\Delta I_{L2}} = \frac{(1-0.52) \times 200}{20000 \times 17 \times 0.06} = 4.7 \times 10^{-3} \approx 5 \text{ mH} \quad (7)$$

$$C_1 = \frac{DI_{dc}}{f_{sw}\Delta V_{C1}} = \frac{0.52 \times 17}{20000 \times 200 \times 0.1} = 22 \mu\text{F} \quad (8)$$

Where  $f_{sw}$  is the switching frequency of IGBT switch of the zeta converter;  $\Delta I_{L1}$  is the amount of permitted ripple in the current flowing through  $L_1$ , same as  $I_{L1} = I_{mpp}$ ;  $\Delta I_{L2}$  is the amount of permitted ripple in the current flowing

through  $L_2$ , same as  $I_{L2}=I_{dc}$ ;  $\Delta V_{C1}$  is permitted ripple in the voltage across  $C_1$ , same as  $V_{C1}=V_{dc}$ .

### C. Estimation of DC-Link Capacitor of VSI

A new design approach for estimation of dc-link capacitor of the VSI is presented here. This approach is based on a fact that sixth harmonic component of the supply (ac) voltage is reflected on the dc side as a dominant harmonic in the three-phase supply system. Here, the fundamental frequencies of output voltage of the VSI are estimated corresponding to the rated speed and the minimum speed of BLDC motor essentially required pumping the water. These two frequencies are further used to estimate the values of their corresponding capacitors. Out of these two estimated capacitors, larger one is selected to assure a satisfactory operation of proposed system even under the minimum solar irradiance level. The fundamental output frequency of VSI corresponding to the rated speed of BLDC motor  $\omega_{rated}$  is estimated as

$$\omega_{rated} = 2\pi f_{rated} = 2\pi \frac{N_{rated} P}{120} = 2\pi \times \frac{3000 \times 6}{120} = 942 \text{ rad/s.} \quad (9)$$

The fundamental output frequency of the VSI corresponding to the minimum speed of the BLDC motor essentially required to pump the water ( $N=1100\text{r/min}$ )  $\omega_{min}$  is estimated as

$$\omega_{min} = 2\pi f_{min} = 2\pi \frac{NP}{120} = 2\pi \times \frac{1100 \times 6}{120} = 345.57 \text{ rad/s} \quad (10)$$

Where  $f_{rated}$  and  $f_{min}$  are fundamental frequencies of output voltage of VSI corresponding to a rated speed and a minimum speed of BLDC motor essentially required to pump the water, respectively, in Hz;  $N_{rated}$  is rated speed of the BLDC motor;  $P$  is a number of poles in the BLDC motor.

The value of dc link capacitor of VSI at  $\omega_{rated}$  is as follows:

$$C_{2,rated} = \frac{I_{dc}}{6 \times \omega_{rated} \times \Delta V_{dc}} = \frac{17}{6 \times 942 \times 200 \times 0.1} = 150.4 \mu\text{F.} \quad (11)$$

Similarly, a value of dc link capacitor of VSI at  $\omega_{min}$  is as follows:

$$C_{2,min} = \frac{I_{dc}}{6 \times \omega_{min} \times \Delta V_{dc}} = \frac{17}{6 \times 345.57 \times 200 \times 0.1} = 410 \mu\text{F} \quad (12)$$

Where  $\Delta V_{dc}$  is an amount of permitted ripple in voltage across dc-link capacitor  $C_2$ . Finally,  $C_2=410\mu\text{F}$  is selected to design the dc-link capacitor.

### D Design of Water Pump

To estimate the proportionality constant  $K$  for the selected water pump, its power-speed characteristics [26], [27] is used as

$$K = \frac{P}{\omega_r^3} = \frac{2.89 \times 10^3}{(2\pi \times 3000/60)^3} = 9.32 \times 10^{-5} \quad (13)$$

Where  $P=2.89 \text{ kW}$  is rated power developed by the BLDC motor and  $\omega_r$  is rated mechanical speed of the rotor (3000r/min) in rad/s.

A water pump with these data is selected for proposed system.

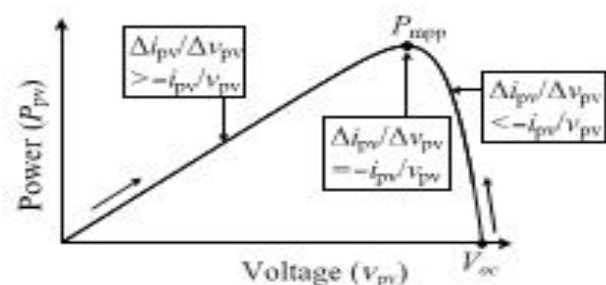


Fig.3. Illustration of INC-MPPT with SPV array  $P_{pv}-v_{pv}$  characteristics.

TABLE.2

Switching States for Electronic Commutation of BLDC Motor

Rotor position $\theta$ (°)	Hall signals			Switching states					
	$H_3$	$H_2$	$H_1$	$S_1$	$S_2$	$S_3$	$S_4$	$S_5$	$S_6$
NA	0	0	0	0	0	0	0	0	0
0-60	1	0	1	1	0	0	1	0	0
60-120	0	0	1	1	0	0	0	0	1
120-180	0	1	1	0	0	1	0	0	1
180-240	0	1	0	0	1	1	0	0	0
240-300	1	1	0	0	1	0	0	1	0
300-360	1	0	0	0	0	0	1	1	0
NA	1	1	1	0	0	0	0	0	0

## V. CONTROL OF PROPOSED SYSTEM

The proposed system is controlled in two stages. These two control techniques, viz., MPPT and electronic commutation, are discussed as follows.

### A. INC-MPPT Algorithm

An efficient and commonly used INC-MPPT technique [8], [13] in various SPV array based applications is utilized in order to optimize the power available from a SPV array and to facilitate a soft starting of BLDC motor. This technique allows perturbation in either the SPV array voltage or the duty cycle. The former calls for a proportional-integral (PI) controller to generate a duty cycle [8] for the zeta converter, which increases the complexity. Hence, the direct duty cycle control is adapted in this work. The INC-MPPT algorithm determines the direction of perturbation based on the slope of  $P_{pv}$ - $v_{pv}$  curve, shown in Fig.3. As shown in Fig.3, the slope is zero at MPP, positive on the left, and negative on the right of MPP, i.e.,

$$\frac{dP_{pv}}{dv_{pv}} = 0; \quad \text{at mpp}$$

$$\frac{dP_{pv}}{dv_{pv}} > 0; \quad \text{left of mpp}$$

$$\frac{dP_{pv}}{dv_{pv}} < 0; \quad \text{right of mpp}$$

Since

$$\frac{dP_{pv}}{dv_{pv}} = \frac{d(v_{pv} * i_{pv})}{dv_{pv}} = i_{pv} + v_{pv} * \frac{di_{pv}}{dv_{pv}} \cong i_{pv} + v_{pv} * \frac{\Delta i_{pv}}{\Delta v_{pv}} \quad (14)$$

Therefore, (14) is rewritten as

$$\left. \begin{aligned} \frac{\Delta i_{pv}}{\Delta v_{pv}} &= -\frac{i_{pv}}{v_{pv}}; && \text{at mpp} \\ \frac{\Delta i_{pv}}{\Delta v_{pv}} &> -\frac{i_{pv}}{v_{pv}}; && \text{left of mpp} \\ \frac{\Delta i_{pv}}{\Delta v_{pv}} &< -\frac{i_{pv}}{v_{pv}}; && \text{right of mpp} \end{aligned} \right\} \quad (16)$$

Thus, based on the relation between INC and instantaneous conductance, the controller decides the direction of perturbation as shown in Fig.3, and increases/decreases the duty cycle accordingly. For instance, on the right of MPP, the duty cycle is increased with a fixed perturbation size until the direction reverses. Ideally, the perturbation stops once the operating point reaches the MPP. However, in practice, operating point oscillates around the MPP. As the perturbation size reduces, the controller takes more time to track the MPP of SPV array. An intellectual agreement between the tracking time and the perturbation size is held to fulfill the objectives of MPPT and soft starting of BLDC motor. In order to achieve soft starting, the initial value of duty cycle is set as zero. In addition, an optimum value of perturbation size ( $\Delta D=0.001$ ) is selected, which contributes to soft starting and also minimizes oscillations around the MPP.

## B. Electronic Commutation of BLDC Motor

The BLDC motor is controlled using a VSI operated through an electronic commutation of BLDC motor. An electronic commutation of BLDC motor stands for commutating the currents flowing through its windings in a predefined sequence using decoder logic. It symmetrically places the dc input current at the center of each phase voltage for  $120^\circ$ . Six switching pulses are generated as per the various possible combinations of three Hall-effect signals. These three Hall-effect signals are produced by an inbuilt encoder according to the rotor position. A particular combination of Hall-effect signals is produced for each specific range of rotor position at an interval of  $60^\circ$  [5], [6]. The generation of six switching states with the estimation of rotor position is tabularized in Table II. It is perceptible that only two switches conduct at a time, resulting in  $120^\circ$  conduction mode of operation of VSI and hence the reduced conduction losses. Besides this, the electronic commutation provides fundamental frequency switching of the VSI; hence, losses associated with high-frequency PWM switching are eliminated. A motor power company makes BLDC motor [28] with inbuilt encoder is selected for proposed system and its detailed specifications are given in the Appendixes.

## VI. FUZZY LOGIC CONTROL

L. A. Zadeh presented the first paper on fuzzy set theory in 1965. Since then, a new language was developed to describe the fuzzy properties of reality, which are very difficult and sometime even impossible to be described using conventional methods. Fuzzy set theory has been widely used in the control area with some application to power system [5]. A simple fuzzy logic control is built up by a group of rules

based on the human knowledge of system behavior. Matlab/Simulink simulation model is built to study the dynamic behavior of converter. Furthermore, design of fuzzy logic controller can provide desirable both small signal and large signal dynamic performance at same time, which is not possible with linear control technique. Thus, fuzzy logic controller has been potential ability to improve the robustness of compensator. The basic scheme of a fuzzy logic controller is shown in Fig 6 and consists of four principal components such as: a fuzzyfication interface, which converts input data into suitable linguistic values; a knowledge base, which consists of a data base with the necessary linguistic definitions and the control rule set; a decision-making logic which, simulating a human decision process, infer the fuzzy control action from the knowledge of the control rules and linguistic variable definitions; a de-fuzzification interface which yields non fuzzy control action from an inferred fuzzy control action [10].

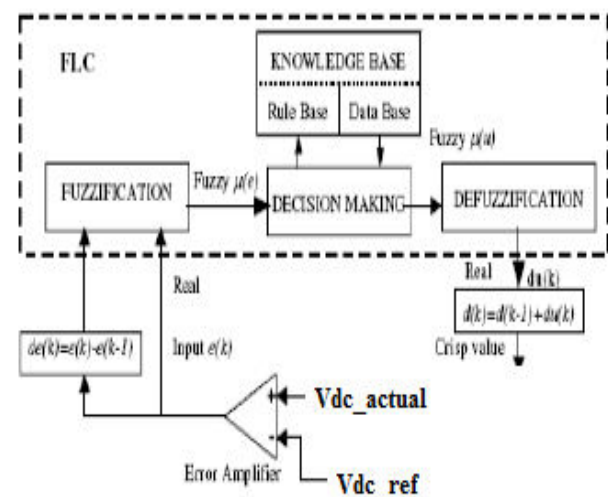


Fig.4. Block diagram of the Fuzzy Logic Controller (FLC) for proposed converter.



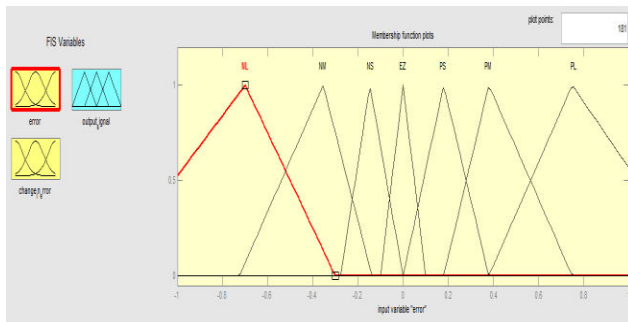


Fig.5. Membership functions for error.

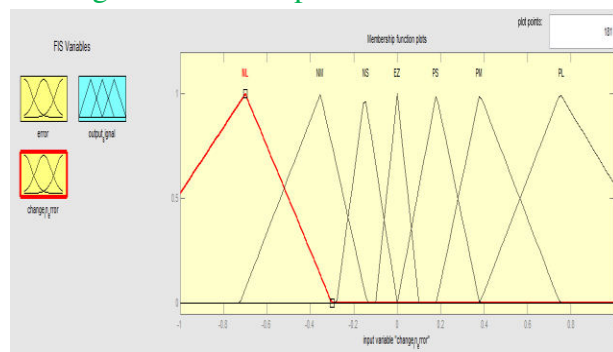


Fig.6. Membership functions for change in error.

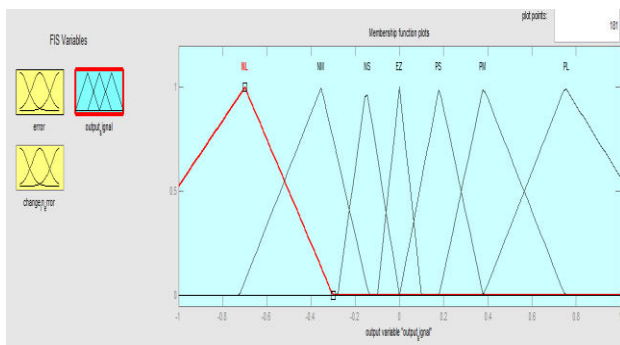


Fig.7. Membership functions for Output.

Error \ Change error	NL	NM	NS	EZ	PS	PM	PL
NL	NL	NL	NL	NL	NM	NS	NL
NM	NL	NL	NL	NM	NS	EZ	NM
NS	NL	NL	NM	NS	EZ	PS	NS
EZ	NL	NM	NS	EZ	PS	PM	EZ
PS	NM	NS	EZ	PS	PM	PL	PS
PM	NS	EZ	PS	PM	PL	PL	PM
PL	EZ	PS	PM	PL	PL	PL	PL

Table 3 Table rules for error and change of error.

## VII. MATLAB/SIMULATION RESULTS

### Case: 1 Steady-State Performance

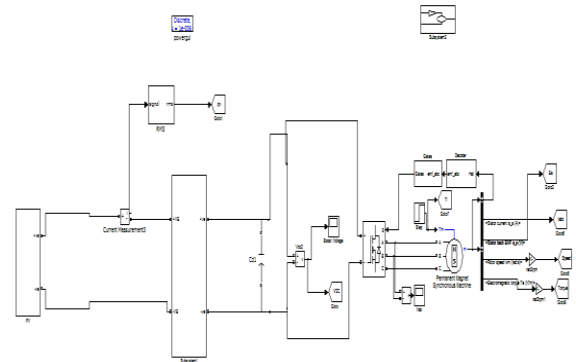
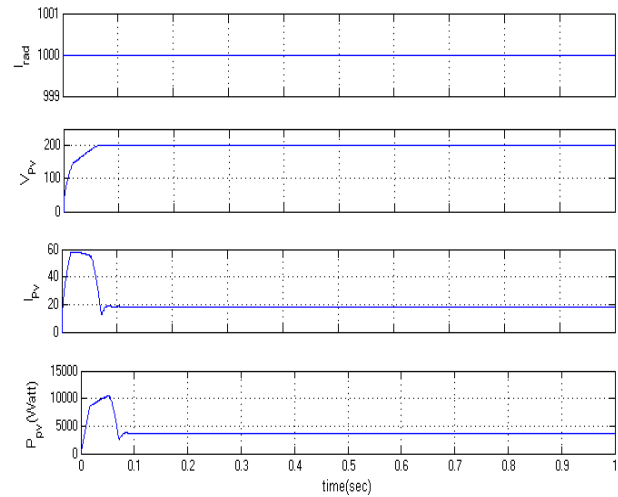
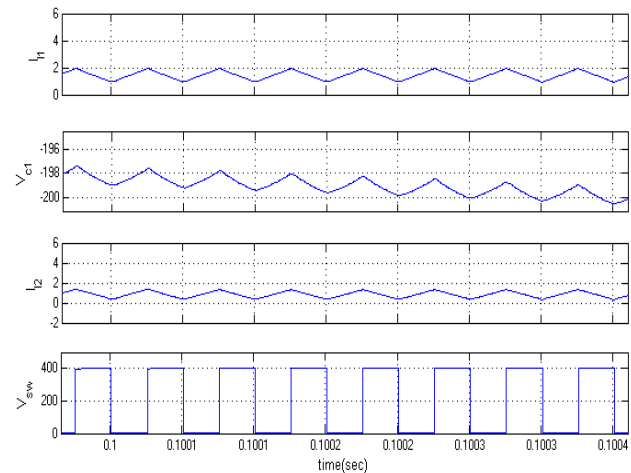


Fig.8 Matlab/Simulink circuit of Starting and steady-state performances of the proposed SPV array based zeta converter-fed BLDC motor drive for water pump



(a)



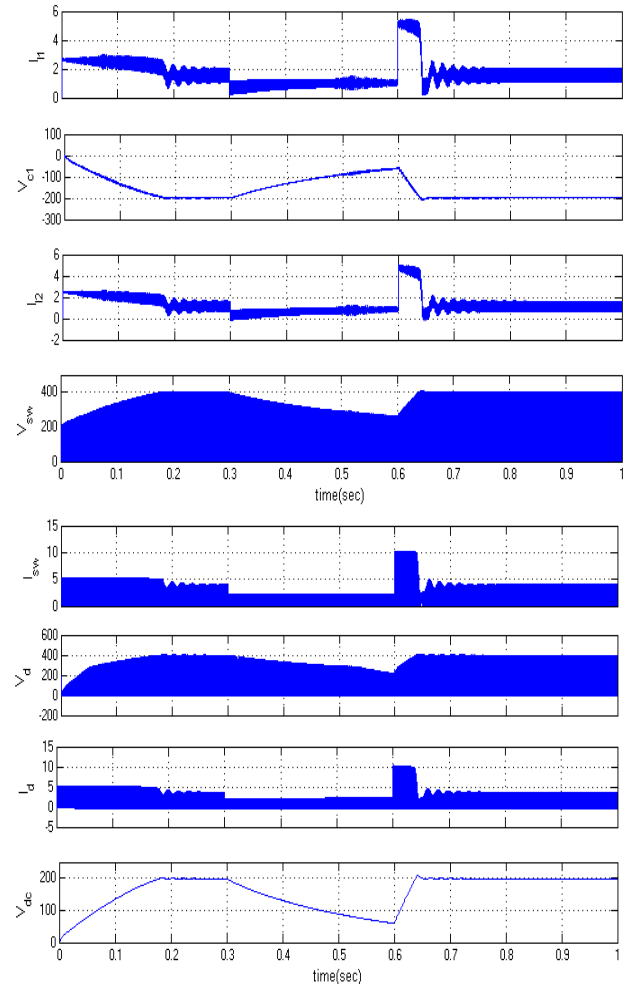
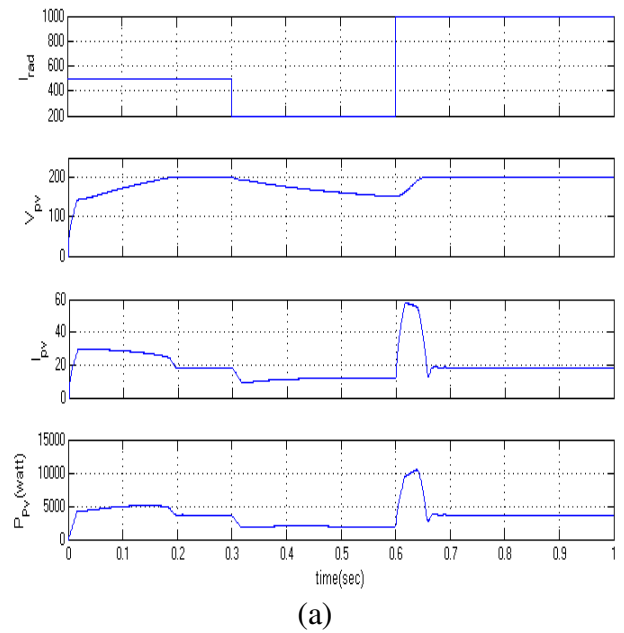
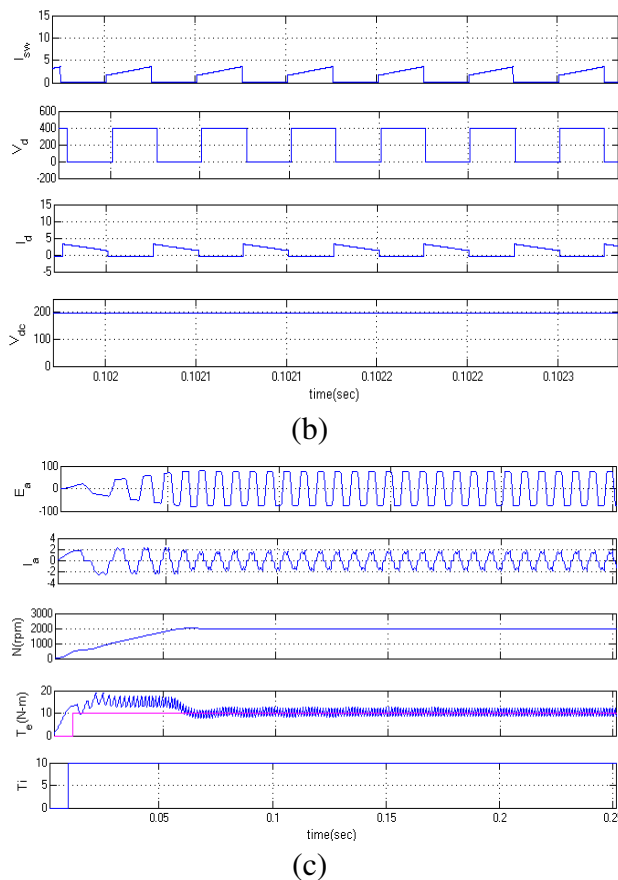


Fig.9 Starting and steady-state performances of the proposed SPV array based zeta converter-fed BLDC motor drive for water pump. (a) SPV array variables. (b) Zeta converter variables. (c) BLDC motor-pump variables.

## Case: 2 Dynamic Performances

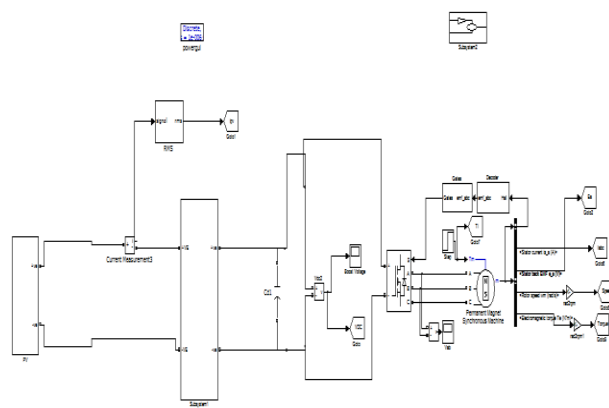


Fig.10 Matlab/Simulink circuit for Dynamic performance of SPV array-based zeta converter-fed BLDC motor drive for water pump

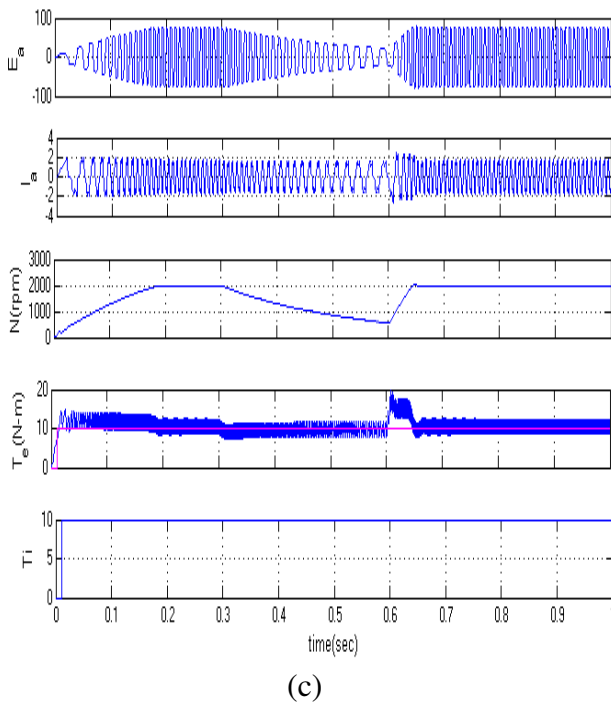


Fig.12 Dynamic performances of the proposed SPV array-based zeta converter-fed BLDC motor drive for water pump. (a) SPV array variables. (b) Zeta converter variables. (c) BLDC motor-pump variables.

### Case: 3 With PI Controller

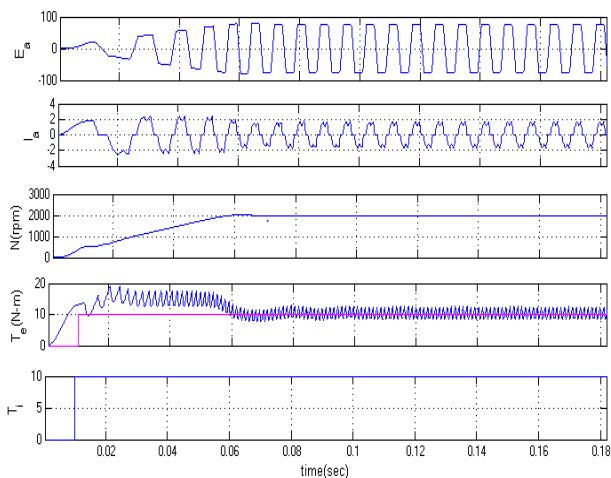


Fig.13 Starting and steady-state performances of the proposed SPV array based zeta converter-fed BLDC motor drive for water pump with PI BLDC Motor Variables.

### Case: 4 With Fuzzy Logic Controller

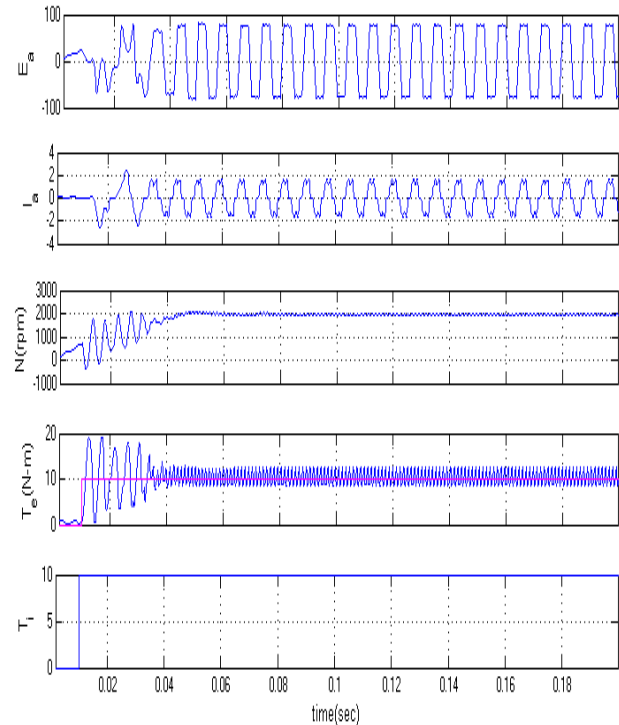


Fig.14 Starting and steady-state performances of the proposed SPV array based zeta converter-fed BLDC motor drive for water pump with Fuzzy BLDC Motor Variables

### VIII. CONCLUSION

The proposed system has been planned and displayed suitably to fulfill the craved goals and approved to look at the different array ions under beginning, dynamic and consistent state conditions. The execution assessment has advocated the blend of zeta converter and BLDC motor for SPV array based water pumping. The system under review has indicated different craved capacities, for example, MPP extraction of the SPV array, delicate beginning of BLDC motor, essential recurrence switching of VSI bringing about a lessened switching losses, speed control of BLDC motor with no extra control. And by using fuzzy controller based BLDC motor can provide an improved speed response and easy to

design effective in dealing with uncertainties. Fuzzy controller based BLDC motor May be referred over PI controller based for automation, robotics, industrial applications.

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