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# PARTICLE SWARM OPTIMIZATION OF AN EXTENDED KALMAN FILTER FOR SPEED ESTIMATION OF PMSM DRIVE USING PARTICLE SWARM OPTIMIZATION

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#### **ABSTRACT**

This paper shows a speed estimation procedure for Permanent Magnet Synchronous Motor (PMSM) in light of Extended Kalman Filter (EKF). Molecule Swarm Optimization (PSO) technique is utilized to improve the clamor covariance networks of EKF, consequently guaranteeing channel dependability and exactness in speed estimation. The proposed strategy will be performed in two stages; in the to start with the covariance grids are upgraded in disconnected way and after that in the second step these mistake covariance frameworks values are infused into EKF to appraise rotor speed. Recreation comes about demonstrates that the covariance frameworks enhance the union of estimation process and nature of the framework execution.

**Keywords:** Permanent Magnet Synchronous Motor, Extended Kalman Filter, Particle swarm optimization, Objective function.

#### 1.INTRODUCTION

Current industry patterns advocate the PMSM as the primary inclination for engine control application planners. Its unparallel highlights, for example, high power thickness, quick unique reaction and high effectiveness in correlation with other engines in its class, together with diminished assembling costs and enhanced attractive properties, make the PMSM a decent suggestion for huge scale item execution [1-2]. Be that as it may, ordinary engine control needs a speed sensor or an optical encoder to gauge the rotor speed with better precision. Sensors introduces a few weaknesses, for example, drive cost, machine unwavering quality size. and clamor invulnerability; along these lines, a sensorless control without position and speed sensors for PMSM drive turn into a well known research theme in writing [3-4]. Different control

calculations like Sliding Mode Observer (SMO) [5], lessened request spectator [6], Full request eyewitness [7], Extended Kalman Filter(EKF) [8-9], Model Reference Adaptive System (MRAS) [10], Fuzzy rationale [11] and Artificial Neural Systems [12] are proposed in the writing for speed and position estimation of PMSM. Among the proposed calculations EKF is one of the promising eyewitnesses, if the commotion covariance grids are known; offers most ideal sifting of the commotion in estimation and of the framework. In the event that the rotor speed considered as an expanded state and is consolidated in the dynamic model of a PMSM then the EKF can be utilized to relinearize the non-direct state show for each new estimation of gauge. Thus, EKF is the best answer for the speed estimation of a PMSM. Yet, EKF estimation for the most part relies



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upon commotion covariance lattices Q and R. They can be acquired by considering the stochastic properties of the comparing clamors. Since these are generally obscure, much of the time the EKF networks are composed what's more, tuned by experimentation systems. Be that as it may, it is a tedious procedure, to conquer this issue the covariance networks are tuned utilizing Genetic calculation [13]. In this paper, another elective technique mix of EKF-PSO is utilized to tune the covariance lattices Q and R. In the initial step, finding the ideal estimations of covariance lattices disconnected technique lastly these qualities are put in the comparing networks and keep running in on-line to appraise rotor speed.

#### 2.MATHEMATICAL MODELING

The voltage equations for a PMSM in the rotor reference frame can be expressed as [14].

$$V_d = R_s i_d + L_d p i_d - \omega_\varepsilon L_g i_g \qquad ---(1)$$

$$V_q = R_s i_q + L_q p i_q + \omega_e L_d i_d + \omega_e \psi_f \qquad ---(2)$$

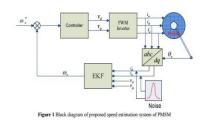
The electromagnetic torque of PMSM is described as

$$T_{e} = \left[ \frac{3}{2} P_{n} i_{q} \left( \psi_{f} - \left( L_{q} - L_{d} \right) i_{d} \right) \right] \qquad --- (3)$$

The motion equation is expressed as follows as

$$J\frac{d\omega_r}{dt} + B\omega_r + T_l = T_e \tag{4}$$

#### 3.PROPOSED SCHEME OF EKF BASED SENSOR LESS SPEED CONTROL OF PMSM DRIVE



#### 3.1 Extended Kalman Filter (EKF)

Kalman Filter is a scientific model that keeps running in parallel to the genuine framework and gives the estimation of the conditions of straight frameworks. In any disadvantage of Kalman channel is that it is a procedure when connected nonlinear frameworks. For the execution of nonlinear frameworks, these elements of the state factors change with each time venture, thus the cycle can't be pre-figured. Deficiencies of this model can be overwhelmed by utilizing Expanded Kalman channel (EKF). In the model portrayed by conditions (1), (2) and (3), the streams of dq-pivot and the speed are chosen as state factors, and the information variable u and yield variable y are characterized as takes after:

$$x = \begin{bmatrix} i_d \\ i_q \\ \omega_r \end{bmatrix}, \ u = \begin{bmatrix} V_d \\ V_q \end{bmatrix}, \ y = \begin{bmatrix} i_d \\ i_q \end{bmatrix}$$

The discrete time system equations are

$$x_k = f_{k-1}(x_{k-1}, u_{k-1}, w_{k-1})$$
 ... (5)  
 $y_k = h_k(x_k, v_k)$  ... (6)

Where xk is state vector, uk is input vector, wk is random state noise, yk is the noisy



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observation or measured variable vector and vk is the measurement noise.

#### 3.2 EKF Algorithm

Step 1: State vector and covariance matrices are initialized

i.e. 
$$x(0)$$
,  $P(0)$ ,  $Q$ ,  $R$ 

Step 2: Find Jacobian matrices  $k \ 1 \ f$  – and  $k \ h$  using

$$F_{k-1} = \frac{\partial f_{K-1}}{\partial x_k} \qquad \qquad \cdots (7)$$

$$H_k = \frac{\partial h_K}{\partial x_k} \qquad \qquad \cdots (8)$$

Step 3: Prediction of state matrix and error covariance matrices

$$x_{k-1} = f_{k-1}(x_{k-1}, u_{k-1}) + x(0)$$
 ... (9)  
 $P_{k-1} = F_{k-1}P_{k-1}F_{k-1}^{T} + Q_{k-1}$  ... (10)

Step 4: Correction state

• Calculation of Kalman gain matrix

$$K_k = P_{k-1}H_k^T / (H_k P_{k-1}H_k^T + R_k)$$
 --- (11)

• Update state prediction

$$x_k = x_{k-1} + K_k (y_k - H_k x_{k-1})$$
 --- (12)

• Estimation of error covariance matrix

$$P_k = (I - K_k H_k) P_{k-1}$$
 --- (13)

#### 3.3 EKF estimation for PMSM drive

The dynamic state equations of PMSM are

$$\frac{di_d}{dt} = \frac{1}{L_d} \left[ -R_s i_d + P_n \omega_r L_q i_q \right] + \frac{V_d}{L_d} \qquad \cdots (14)$$

$$\frac{diq}{dt} = \frac{1}{L_a} \left[ -R_s i_q - P_n W_r L_d i_d - P_n \omega_r \psi_f \right] + \frac{V_q}{L_a} \qquad --- (15)$$

$$\frac{d\omega r}{dt} = \frac{1}{J} \left[ \frac{3}{2} P_{a^{\dagger}q} \left( \psi_f - \left( L_q - L_d \right) i_d \right) \right] - \frac{B}{J} \omega_r - \frac{T_I}{J} \qquad \cdots (16)$$

The above equations written in the form of state space representation

$$\begin{bmatrix} \frac{di_d}{dt} \\ \frac{di_q}{dt} \\ \frac{d\theta_r}{dt} \end{bmatrix} = \begin{bmatrix} \frac{-R_s}{L_d} & \frac{P_n \omega_r L_q}{L_d} & 0 \\ \frac{-P_n \omega_r L_d}{Lq} & \frac{-R_s}{L_q} & \frac{-P_n \psi_f}{L_q} \\ \frac{-3P_n \left(L_q - L_d\right) i_q}{2J} & \frac{3P_n \psi_f}{2J} & \frac{-B}{J} \end{bmatrix} \begin{bmatrix} i_d \\ i_q \\ \omega_r \end{bmatrix} + \begin{bmatrix} \frac{1}{L_d} & 0 \\ 0 & \frac{1}{L_q} \\ 0 & 0 \end{bmatrix} \begin{bmatrix} V_d \\ V_q \end{bmatrix} \qquad \cdots (17)$$

Discrete time representation of above equation is

$$f_{k-1}(x_{k-1}, u_{k-1}, w_k) = \begin{bmatrix} 1 - \frac{R_s}{L_d} T_s & \frac{P_n \omega_r L_q}{L_d} T_s & 0 \\ -\frac{P_n \omega_r L_d}{L_q} T_s & 1 - \frac{R_s}{L_q} T_s & -\frac{P_n w_f}{L_q} T_s \\ \frac{-3P_n \left(L_q - L_d\right) i_q}{2J} T_s & \frac{3P_n w_f}{2J} T_s & 1 - \frac{B}{J} T_s \end{bmatrix} \begin{bmatrix} i_d \\ i_q \\ \omega_r \end{bmatrix} + \begin{bmatrix} \frac{1}{L_d} T_s & 0 \\ 0 & \frac{1}{L_q} T_s \\ 0 & 0 \end{bmatrix} \begin{bmatrix} V_d \\ V_q \end{bmatrix}$$
 --- (18)

The Gradient matrix is given as

$$F_{k-1} = \frac{\partial f_{K-1}}{\partial x_k} = \begin{bmatrix} 1 - \frac{R_s}{L_d} T_s & \frac{P_n \omega_r L_q}{L_d} T_s & 0 \\ -\frac{P_n \omega_r L_d}{L_q} T_s & 1 - \frac{R_s}{L_q} T_s & \frac{-P_n \psi_f}{L_q} T_s \\ -\frac{3P_n \left( L_q - L_d \right) i_q}{2J} T_s & \frac{3P_n \psi_f}{2J} T_s & 1 - \frac{B}{J} T_s \end{bmatrix}$$
 --- (19)

$$H_k = \frac{\partial h_K}{\partial x_k} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \end{bmatrix}$$
 --- (20)



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# 4. PARTICLE SWARM OPTIMIZATION (PSO)

Molecule swarm streamlining, a swarm knowledge based worldwide arbitrary pursuit calculation, is proposed by Kennedy and Eberhart propelled from manufactured life explore comes about [15]. It respects all people in the populace as particles without mass and volume in the D-dimensional pursuit space and every molecule moves at a specific speed to the best position of its own history Pbest and the best position of its neighborhood history gbest in the arrangement space, keeping in mind the end goal to accomplish the advancement of hopeful arrangements.

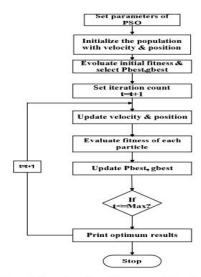


Figure 2 Flow chart of particle swarm optimization

# 5. TUNING OF EKF USING PARTICLE SWARM OPTIMIZATION

The basic advance in a Kalman channel configuration is to get a numerical assessment of the channel parameters determined by the introductory state x (0), and the covariance networks P(0), Q and R. This procedure is called tuning and it includes an iterative scan

for the coefficient esteems that yield the most ideal estimation execution. Changing the covariance networks Q and R influences both the transient and the relentless state operation of the channel. Expanding Q would show increment in either clamor driving the framework or vulnerability in the model. This will build the estimations of the state covariance components. The channel additions will likewise increment along these lines weighting the estimations all the more intensely, and the channel transient execution is quicker. Correspondingly, expanding covariance R shows that the estimations are subjected to a more grounded corruptive clamor and ought to be weighted less by the channel. Therefore the estimations of the pick up framework K will diminish, and the transient execution is slower. For underlying state covariance network Po, the slanting terms speak to fluctuations or mean squared mistakes in learning of the underlying conditions. Shifting P (0) yields an alternate extent transient trademark. The transient term will be the same and the relentless state conditions are unaffected. The covariance networks Q, R and P (0) are thought to be inclining because of need of adequate factual data to assess their off-askew terms. The principle target capacity of this paper is determination of ideal estimations of Q and R. These qualities are chosen physically by utilizing trial and mistake strategy. However, this is extremely tedious process. To surmount this issue, covariance frameworks are tuned by utilizing Particle Swarm Advancement (PSO).

The objective function F= w1e1+w2e2+w3e3



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Where

$$e_1 = \int (i_{d-act} - i_{d-est})^2$$

$$e_2 = \int (i_{q-act} - i_{q-est})^2$$

$$e_3 = \int (\omega_{r-act} - \omega_{r-est})^2$$

Proper selection of weights is essential in tuning else these weights may lead to large errors. These weights are selected as follows w1=0.125, w2=0.05, w3=0.00167.

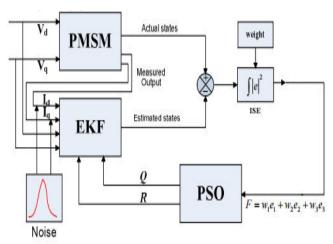


Figure 3 EKF-PSO block diagram

#### 6. RESULTS AND DISCUSSIONS

In the simulation d i , q i , d v , q v are input variables of EKF algorithm and d i , q i , $\omega$ r are the estimated state variables. In order to mimic the condition of real system Gaussian white noises are added to feedback values of d i , q i are set to  $3\times10$ -6 and sample time of the white noise block is set to  $2\times10$ -5 sec. It should be noted that the convergence of the PSO method to the optimal solution depends on the parameters c1, c2, wmin, and wmax values. During the simulation, these values are set to

c1=2, c2=2, wmin,=0.5 and wmax =0.9 respectively

Table 1: PSO-EKF estimations

Number of iterations = 50(PSO)				
Number of	Diagonal matrix Q	Diagonal matrix R	Objective	
Generations			function value	
5	[18.6932 6.4571 95.5391]	[1319.2855 1255.226]	0.0341	
10	[21.8921 4.3835 111.8467]	[4294.768 1745.057]	0.0337	
20	[47.8346 7.2033 131.0535]	[1220.123 2067.458]	0.0320	

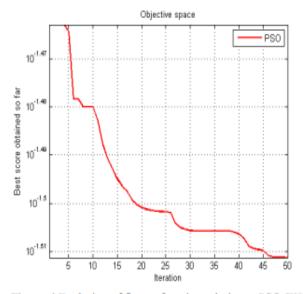


Figure 4 Evolution of fitness function relative to PSO-EKF

Optimized parameters of matrices Q & R of EKF with their corresponding ISEs obtained by proposed PSO-EKF method and its performance is given in Figure 4. Table 1 shows the convergence of PSO-EKF process and ISE is decreased with increasing of generation count. Here best objective function value is obtained for generation count 20, corresponding values are injected into EKF and run in online manner. Finally the states of the EKF is estimated as shown in below figures.



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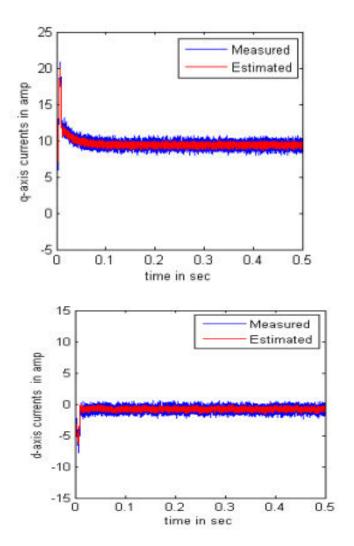


Figure 5 Measured and estimated current of  $i_{\boldsymbol{q}}$  and  $i_{\boldsymbol{d}}$ 

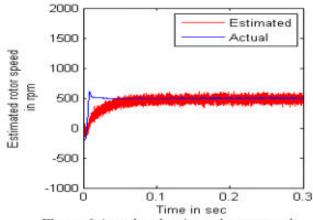
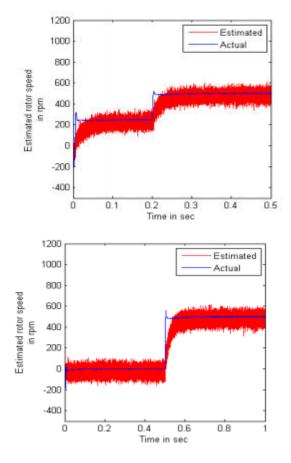


Figure 6 Actual and estimated rotor speed



**Figure 7** Actual and estimated rotor speed under variable speeds

The measured and estimated waveforms of id and iq are shown in figure 5. Due to convergence problem of state covariance matrix P, the estimated dq-axes currents having large ripples upto 0.03 sec. After 0.03 sec matrix P is converges, then state variables id and iq are tracks the actual values. From Figure 6 it is evident that the estimated speed matches with the actual speed near 0.001 sec. The effectiveness of PSO-EKF method is evaluated under two cases, in one case the speed is varied from 200 rpm to 500 rpm at 0.5 sec and in another case motor is run at 500 rpm at 0.5 sec as shown in figure 7 and in both cases the



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estimated speed is converged accordingly due to precise values of matrices Q & R.

#### 7. CONCLUSION

In this paper, EKF based sensorless speed control of PMSM drive has been exhibited to demonstrate the aftereffects of assessed estimations of speed and dq-tomahawks stator streams. The execution of EKF is for the most part relies upon blunder covariance lattices Q and R, which are reasonably chosen. These grids are enhanced the framework union and nature of estimation. The reproduction comes about demonstrate the predominant execution as far as settling time, lessening of commotion and general framework strength.

#### Appendix A:

Simulation Parameters values of PMSM drive:

Parameters	Symbol	Numerical value
Resistance of stator	R <sub>s</sub>	0.675 ohm
Direct axis inductance of stator	L <sub>d</sub>	0.0085 H
Quadrature axis inductance of stator	Lq	0.0085 H
Flux linkages	$\psi_{\rm f}$	0.12 Wb
Inertia of rotor	J	0.0011 Kg/m <sup>2</sup>
friction coefficient	В	0.0014 Nm/s <sup>2</sup>
Pair of poles	P <sub>n</sub>	3
Rated speed	ω	1000 rpm

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